

METHOD AND APPARATUS FOR INSPECTING TARGET

BY TERA-HERTZ WAVE SPECTROMETRY

BACKGROUND OF THE INVENTION

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Field of the Invention

The present invention relates to a method and apparatus for inspecting a target by tera-hertz wave spectrometry.

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Description of the Related Art

A frequency of a far infrared ray or submillimeter wave which ranges about from 0.5 to 3 THz is positioned at the boundary between the frequency range of a light wave and the frequency range of a radio wave. The technology for a light wave and the technology for a radio wave have been advanced respectively. On the other hand, the technology for a far infrared ray or submillimeter wave has not been cultivated from the standpoint of technical advancement and its technical application. However, recently, it is becoming more important to effectively use the frequency range of about 0.5 to 3 THz in radio communication, apply this frequency range to ultrahigh-speed communication, and take advantage of characteristics of an electromagnetic wave of this frequency region for inspecting environment by imaging or tomography. In the following, this frequency region (about 0.5 to 3 THz) of a

far infrared ray or submillimeter wave is referred to as a tera-hertz wave.

Patent Literatures 1 and 2, for example discloses means for generating a tera-hertz wave. Non-Patent 5 Literatures 1, 2 and 3 are other documents related to a tera-hertz wave.

[Non-Patent Literature 1]

S.Kawata, K.Sasaki, and S.Minami, "Component analysis of spatial and spectral patterns in multispectral images.

10 I.Basis," J.Opt.Soc.Am.A4, 2101(1987).

[Non-Patent Literature 2]

K.Sasaki, S.Kawata, and S.Minami, "Component analysis of spatial and spectral patterns in multispectral images.

II. Entropy minimization," J.Opt.Soc.Am.A6, 73(1987).

15 [Non-Patent Literature 3]

S.Kawata, and S.Minami, "Image Process for Scientific Instrument", Chapter 11, Color Image and Image Spectroscopy, Publisher CQ, P259-265.

[Non-Patent Literature 4]

20 Izumi Yoshiharu, "Guidance for Equipment Analysis", Chapter 1, Infrared Absorption Spectrum Method", Kagaku Dojin P1-20.

[Patent Literature 1]

Japanese Laid-Open Patent Publication No. 2002-72269

25 [Patent Literature 1]

Japanese Laid-Open Patent Publication No. 2003-5238

One of characteristics of a tera-hertz wave is that the wavelength is not only within the range of the shortest wavelength of a radio wave that propagates through a material, but also within the region of the longest wavelength of a light wave that propagates straight. In other words, a tera-hertz wave can penetrates through various materials like a radio wave, and provide the highest space resolution in a radio wave, and be guided by a lens or mirror like a light wave.

Thus, a tera-hertz wave can penetrates through a semiconductor, plastic, paper, rubber, vinyl, wood, textile, ceramics, concrete, a tooth, a bone, fat, dried food, ice, and so on. For this reason, a tera-hertz wave is expected as imaging means that is an alternative to a X-ray and is safe for a human body.

Recently, one of a terrorist act that anthrax bacteria or drug is distributed by mail was raised as a social problem. The shape of an object enclosed in an envelope can be determined by conventional X ray, but the property of the object in the envelope cannot be determined unless the envelope is opened. Accordingly, when powdery anthrax bacteria or drug is enclosed in an envelope, any abnormality cannot be detected by X ray photograph.

SUMMARY OF THE INVENTION

The present invention was made to solve the above problems. That is, it is an object of the present 5 invention to provide a target inspecting method and apparatus that can determine the contents component inside a mail article or the like and the shape of the contents that were not determined by a conventional X ray photograph, without opening the mail article.

10 According to the present invention, there is provided a method of inspecting a target by tera-hertz wave spectroscopic measurement, comprising:

15 a spectroscopic measurement step of pre-measuring a spectrum [S] of tera-hertz wave absorbencies of a target component for a plurality of frequencies ranging about from 1 THz to 3 THz; and

20 an object spectroscopic step of irradiating an object with tera-hertz waves of the plurality of frequencies to measure absorbencies I of the object, wherein presence and absence of the target component in the object is determined on the basis of the spectrum [S] of the absorbancy S and the spectrum [I] of the absorbancy I of the object.

25 According to a preferred embodiment of the present invention, the method comprises a density calculation step of calculating a target density [P] on the basis of the

spectrum [S] of the absorbancy S and the spectrum [I] of the absorbancy I of the object.

Further, the target spectroscopic step comprises a step of two-dimensionally scanning the object with the 5 tera-hertz waves to measure a two-dimensional distribution [I] of the absorbancy I of penetration light, and the density calculation step comprises a step of calculating a two-dimensional distribution [P] of the target density P.

Furthermore, according to the present invention, 10 there is provided an apparatus for inspecting a target using tera-hertz wave spectroscopic measurement, comprising:

a tera-hertz wave generation device (12) that generates tera-hertz waves (4) of a plurality of 15 wavelengths;

a two-dimensional scan device (18) that scans an object (10) with the tera-hertz waves of the plurality of wavelengths,

a spectroscopic measurement device (14) that measures 20 a two-dimensional distribution [I] of light absorbancy I of the object; and

a target density calculation device (16) that calculates a two-dimensional distribution [P] of a target density P on the basis of a pre-measured spectrum [S] of 25 light absorbancy S of a target and the two-dimensional distribution [I] of the light absorbancy I.

By the above method and apparatus, tera-hertz waves (4) of a plurality of different wavelengths are generated by the tera-hertz wave generation device (12), the object (10) is scanned with the terahertz waves (4) by the two-dimensional scan device (18), and the two-dimensional distribution [I] of the absorbancy I of the object is measured by the spectroscopic measurement device (14) so that the two-dimensional distribution [P] of the target density P can be calculated on the basis of the pre-measured spectrum [S] of the absorbancy S of the target and the two-dimensional distribution [I] of the absorbancy I by imaging spectroscopy, using the target density calculation apparatus.

Accordingly, it is possible to determine the component of the contents inside a mail article or the like without opening the mail article when the component has a tera-hertz wave absorbancy depending on the wavelength. Furthermore, it is possible to determine abnormality of the inside contents that was not determined by a conventional x-ray photograph.

In addition, the apparatus comprises an image display device (20) that two-dimensionally displays an image of the two-dimensional distribution [P] of the target density P. The image of the two-dimensional distribution [P] of the target density P is two-dimensionally displayed so that the shape of the target having a wavelength-dependent property

in the object (10) can be two-dimensionally displayed together with the distribution of the target.

The tera-hertz waves of N number of different wavelengths are used for M number of targets, N being equal 5 to or larger than M, when N is equal to M, the two-dimensional distribution [P] of the target density P is calculated by $[P] = [S]^{-1}[I]$, and when N is larger than M, the two-dimensional distribution [P] of the target density P is calculated by $[I] = [S][P]$, using a least square 10 method.

Thereby, even when a plurality of targets exist, the shapes of the targets having the wavelength-dependent property in the object (10) as well as the distributions of the targets can be two-dimensionally displayed in a short 15 time by processing the image of the two-dimensional distribution [I] of the light absorbancy, using a general-purpose personal computer.

Other objects and advantageous features of the present invention will become apparent from the following 20 description with reference to the accompanying drawings.

BRIEF DESCRIPTION OF DRAWINGS

FIG. 1 shows a principle of generation of a tera-25 hertz wave;

FIG. 2 shows the configuration of a tera-hertz wave

generation device having a resonator;

FIG. 3 shows the entire configuration of a target inspecting apparatus according to the present invention;

FIG. 4 shows the relation between the frequency of a 5 tera-hertz wave and the light absorbancy of a target;

FIG. 5 schematically shows objects according to an embodiment of the present invention;

FIGS. 6A through 6I show penetration images captured for different frequencies of a tera-hertz wave;

10 FIGS. 7A through 7D show density distributions of respective materials obtained from the 6 images of FIGS. 6A through 6I.

DESCRIPTION OF THE PREFERRED EMBODIMENTS

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In the following, a preferred embodiment of the present invention will be described with reference to the drawings. In the drawings, the same reference numeral is attached to the common parts, and the overlapping 20 description will be omitted.

FIG. 1 shows a principle of tera-hertz wave generation. In FIG. 1, the reference numeral 1 designates a nonlinear optical crystal (for example, LiNbO₃), the reference numeral 2 a pump wave (for example, YAG laser beam), the reference numeral 3 a idler wave, and the 25 reference numeral 4 a tera-hertz wave.

When the pump wave 2 enters, in a certain direction, the nonlinear optical crystal 1 having Raman activity and far infrared activity, the idler wave 3 and the tera-hertz wave 4 are generated via an elementary excitation wave 5 (polariton) of the material by induced Raman effect (or the parametric interaction). In this case, an energy conservation law expressed by the equation (1) and a momentum conversation law expressed by the equation (2) are established among the pump wave 2 (ω_p), the tera-hertz 10 wave 4 (ω_t), and the idler wave 3 (ω_i). In the equation (2), each term is a vector, and the non-collinear phase matching condition can be expressed as indicated by the illustration at the upper right in FIG. 1.

$$\omega_p = \omega_t + \omega_i \dots (1)$$

15 $\kappa_p = \kappa_t + \kappa_i \dots (2)$

The generated idler wave 3 and the tera-hertz wave 4 have spatial extent, and the wavelengths of the idler wave 3 and the tera-hertz wave 4 continuously vary in accordance with the output angle. The generation of this 20 broad idler wave 3 and tera-hertz wave 4 in the single path arrangement is referred to as TPG (THz-wave Parametric Generation).

The basic parametric process is defined by extinction of one pump photon, and the simultaneous generation of one 25 idler photon and one signal photon. When the idler light or the signal light resonates, and the intensity of the

pump light exceeds a threshold value, parametric generation occurs. The induced Raman scattering is defined by the extinction of one pump photon, the simultaneous generation of one idler photon and one polariton. The induced Raman 5 scattering is included in the broad-defined parametric interaction.

However, the tera-hertz wave generated by a tera-hertz wave generation device of the single path arrangement is very weak. Furthermore, a large part of the generated 10 tera-hertz wave is absorbed when the tera-hertz wave advances in the nonlinear optical crystal by several-hundred microns.

FIG. 2 shows the configuration of a tera-hertz wave generation device that solves this problem. As shown in 15 FIG. 2, the resonator is arranged in the specific direction (angle θ) relative to the broad idler wave 3 so as to increase the intensity of the idler wave 3 in the specific direction. In this case, the resonator includes mirrors M1 and M2 having high reflective coats, and is disposed on a 20 rotary stage 5 such that the angles of the resonator can be adjusted. The high reflective coat is formed on one half part of each of the two mirrors M1 and M2 such that the pump wave 2 can penetrate through the other half of each of the mirrors M1 and M2. In FIG. 2, the reference numeral 6 25 designates a prism coupler for extracting the tera-hertz wave 4 to the outside.

In the tera-hertz wave generation device shown in FIG. 2, when an incident angle θ of the pump wave to the crystal is changed within a certain range (for example, 1 to 2 degrees), an angle of the pump wave made with the 5 idler wave is changed, and an angle of the tera-hertz wave made with the idler wave is also changed. By this phase matching condition change, the wavelength of the tera-hertz wave can be continuously changed between about 140 microns to about 310 microns, for example.

10 FIG. 3 shows the entire configuration of a target inspecting apparatus according to the preferred embodiment of the present invention. In FIG. 3, the target inspecting apparatus includes the tera-hertz wave generation device 12, a spectroscopic measurement device 14, a target density 15 calculation device 16, a two-dimensional scan device 18, and an image display device 20.

The tera-hertz wave generation device 12 includes the nonlinear optical crystal 1 capable of generating the tera-hertz wave by the parametric effect, a pump wave 20 introducing device that introduces the pump wave 2 to the nonlinear optical crystal 1 to generate the idler wave 3 and the tera-hertz wave 4, and a switching device 13 that changes the wavelength of the generated tera-hertz wave 4.

25 In this example, the tera-hertz wave generation device 12 is the tera-hertz wave generation device shown in FIG. 2. In this example, the switching device 13 a rotary

stage that rotates a stage on which the mirrors M1 and M2 are disposed so as to change the incident angle θ of the pump light to the crystal.

According to the tera-hertz wave generation device 12, 5 operating the switching device 13 (the rotary stage) enables the generation of the tera-hertz waves having different wavelengths in the tera-hertz region of about 1 THz to 3 THz.

In FIG. 3, the spectroscopic measurement device 14 10 includes a divider 14a, a condenser lens 14b, and a spectroscopic measurement unit 15.

The divider is a wire grid in this example, and divides the tera-hertz wave 4 into measurement light 4a and reference light 4b at a predetermined ratio. The 15 measurement light 4a is introduced to the condenser lens 14b via reflective mirrors 17a and 17b. The reference light 4b is introduced to the spectroscopic measurement unit 15 via a reflective mirror 17c. The condenser lens 14b condenses the measurement light 4a on an object, and 20 the measurement light 4a that has penetrated through the object reaches a scattering lens 14c where the diameter of the measurement light is enlarged. Then, the measurement light 4a is introduced to the spectroscopic measurement unit 15. The condenser lens 14b and the scattering lens 25 14c are TPX lenses having a focal length of about 30 mm. The spectroscopic measurement device 15 is a Si bolometer

having two built-in detection elements, for example. The output of the spectroscopic measurement unit 15 is input to the target density calculation device 16.

5 The target density calculation device 16 is a personal computer having a storage unit, for example, and calculates the two-dimensional distribution of a target density on the basis of the pre-measured spectrum [S] of the light absorbancy S of a target and the two-dimensional distribution [I] of the light absorbancy I.

10 Even when the output fluctuation (ΔI) of the tera-hertz wave 4 exists, the output fluctuation (ΔI) is automatically compensated by using the reference light 4b. Thereby, the output fluctuation is corrected to always obtain accurate transmissivity of the object 10.

15 When the object 10 is a mail article, paper, plastic or textile that is the general internal contents of the mail article does not have tera-hertz wave absorption property that depends on the wavelength, that is, such general contents absorbs the tera-hertz wave at the same 20 absorption rate for the different wavelengths.

On the other hand, a drug such as aspirin and vitamin, and bio-powder such as anthrax bacteria have the tera-hertz wave absorption property that depends on the wavelength, and absorbs the tera-hertz wave at the different absorption 25 rates for the different wavelengths. Although the reason for this fact is not obvious, the reason is considered to

be that the vibration frequency resulting from the molecular structure is close to the band of the tera-hertz wave.

Accordingly, on the basis of the difference in the transmissivity, the target density calculation device 16 can detect presence or absence of the target that has the tera-hertz wave absorption property depending on the wavelength. In the case of detecting the target that has the tera-hertz wave absorption property depending on the wavelength, this target can be opened in a safe apparatus to be examined.

The two-dimensional scan device 18 moves the object 10 in a x-y plane, for example, and two-dimensionally scans the surface of the object with the tera-hertz waves of a plurality of different wavelengths. The image display device 20 two-dimensionally displays the position detected by the target density calculating device 16 where the transmissivity is different between two wavelengths.

A method according to the preferred embodiment of the present invention uses the above-described target inspecting apparatus, and includes a spectrometric measurement step (A), an object spectrometric step (B), and a density calculation step (C).

At the spectrometric measurement step (A), the spectrum [S] of the absorbancy S is pre-measured for different wavelengths of about 1 THz to 3 THz, and the pre-

measured spectrum [S] is stored.

At the spectrometric measurement step (B), the object is irradiated with the tera-hertz waves of the respective wavelengths to measure the absorbancy I of the object. At 5 this step (B), it is preferable to two-dimensionally scan the object with the tera-hertz wave to measure the two-dimensional distribution [I] of the absorbancy I for the penetration light.

At the density calculation step (C), the target 10 density P is calculated on the basis of the spectrum [S] of the absorbancy S and the absorbancy I. In the case of measuring the two-dimensional distribution [I] of the absorbancy I for the penetration light, the two-dimensional distribution [P] of the target density P is calculated at 15 this step (C). The calculated two-dimensional distribution [P] of the target density P is two-dimensionally displayed by the image display device 20.

FIG. 4 shows the relation between the frequency of the tera-hertz wave and the absorbancy S of the target. In 20 FIG. 4, the horizontal axis designates the frequency of the tera-hertz wave (THz), and the vertical axis designates the absorbancy $\log(I/I_0)$ that is logarithm of the tera-hertz wave intensity I divided by the incident intensity.

As indicated by "D" in FIG. 4, when a sample is the 25 general contents (paper, plastic or textile, for example) of a mail article, the attenuation (i.e., absorbancy) is

almost constant.

Meanwhile, in FIG. 4, the transmissivity (absorbancy) change against the frequency (inverse number of wavelength) is different between 5-aspirin (A), palatinose (B) and 5 riboflavin (C). Thus, FIG. 4 shows the tera-hertz wave absorption property depending on the wavelength. In the present invention, a material that exhibits such absorption property depending on the wavelength is a detection target.

A principle of the present invention will be 10 described.

For the simplest example, it is assumed that the densities of two materials A and B having wavelength-dependent property are P_A and P_B , respectively, the transmissivities of the material A for the wavelengths λ_1 and λ_2 are $S_A(\lambda_1)$ and $S_A(\lambda_2)$, respectively, and the transmissivities of the material B for the wavelengths λ_1 and λ_2 are $S_B(\lambda_1)$ and $S_B(\lambda_2)$, respectively. In this case, the absorbencies I_1 and I_2 of the penetration light of the wavelengths λ_1 and λ_2 are expressed by the equations (3) 15 and (4).

$$I_1 = S_A(\lambda_1)P_A + S_B(\lambda_1)P_B \dots (3)$$

$$I_2 = S_A(\lambda_2)P_A + S_B(\lambda_2)P_B \dots (4)$$

In the equations (3) and (4), if I_1 , I_2 , $S_A(\lambda_1)$, $S_A(\lambda_2)$, $S_B(\lambda_1)$, and $S_B(\lambda_2)$ are known, the densities P_A and P_B of 25 the two materials A and B can be obtained by solving the above simultaneous equations.

Similarly, it is assumed that the two-dimensional distributions of the densities of M number of materials are expressed by a matrix $[P]$, the spectra of the absorbancies S against N number of different wavelengths for the 5 respective materials are expressed by a matrix $[S]$, and the two-dimensional distributions of the transmissivities of the penetration light against the respective wavelengths (frequencies) are expressed by a matrix $[I]$. On this assumption, the equation (5) can be established.

10 $[I] = [S][P] \dots (5)$

In this case, the image obtained by the tera-hertz waves of N frequencies can be expressed by a linear determinant as shown in the equation (6).

[Formula 1]

$$\begin{bmatrix} I(1,1) & \dots & I(1,L) \\ \vdots & & \vdots \\ I(N,1) & \dots & I(N,L) \end{bmatrix} = \begin{bmatrix} S(1,1) & \dots & S(1,M) \\ \vdots & \dots & \vdots \\ S(N,1) & \dots & S(N,M) \end{bmatrix} \begin{bmatrix} P(1,1) & \dots & P(1,L) \\ \vdots & & \vdots \\ P(M,1) & \dots & P(M,L) \end{bmatrix} \quad (6)$$

15

In the equation (6), $[I]$ is a matrix formed by horizontally arranging a one-dimensionally row vector $I(f_1)$, $I(f_2)$, \dots $I(f_N)$, $[P]$ is a matrix formed by vertically 20 arranging the spectra of the respective materials, and $[P]$ is a matrix formed by horizontally arranging vector expressions P_1 , P_2 , \dots P_N for the respective material patterns. In the equation (6), "L" designates the size of the image.

25 If $[S]$ and $[I]$ are known, $[P]$ can be obtained from

the equation (6).

In other words, in the case of $N = M$, the two-dimensional distributions $[P]$ of the target densities P can be obtained by the equation $[P] = [S]^{-1}[I]$. Further, in the 5 case of $N > M$, the two-dimensional distributions $[P]$ can be calculated by the equation $[I] = [S][P]$, using the least square method as shown in the equation (7).

[Formula 2]

$$[P] = ([S]'[S])^{-1}[S]'[I] \quad \dots (7)$$

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[Embodied Example]

In the following, an embodied example of the present invention will be described.

5 pieces of samples (pellets) were prepared as target 15 materials by selecting palatinose and 5-aspirin shown in FIG. 4. The three of 5 pellets were mixtures of palatinose and polyethylene powder with the densities of palatinose being 50 percents, 40 percents and 20 percents, respectively. The other two of 5 pellets were mixtures of 20 5-aspirin and polyethylene powder with the densities of 5-aspirin being 50 percent and 20 percent, respectively. Each of 5 pellets had the same thickness of 1 mm and the same weight of 0.2 g. The 5 pellets as the objects 10 were attached on a thin plastic plate by a two-sided tape as 25 shown in FIG. 5.

The relation spectra $[S]$ between the wavelength

(frequency) and absorbancy was measured for the pellets having the densities of 50 percents in the tera-hertz region of about 1.2 THz to 2.0 THz. The measured relation spectra were stored in the memory of the computer. These 5 tera-hertz spectroscopic property were the same as shown in FIG. 4.

Next, by using the device shown in FIG. 3, the objects 10 were two-dimensionally scanned with the tera-hertz wave of 1.2 THz to 2.0 THz to measure the two-10 dimensional distributions of the absorbancies of the objects 10. The measured distributions were stored in the memory of the computer, and were displayed on the image display device 20.

FIGS. 6A through 6I show the penetration images of 15 the objects 10 for the different frequencies. The scale for these images is the logarithm of the penetration tera-hertz wave intensity I divided by the incident tera-hertz wave intensity. It can be understood that dark and light coloring of these images of the 5 pellets is different 20 between 1.2 THz, 1.3 THz, 1.4 THz, 1.5 THz, 1.6 THz, 1.7 THz, 1.8 THz, 1.9 THz and 2.0 THz.

FIGS. 7A through 7D show density distributions of 25 each material obtained from the 6 images of FIGS. 6B through 6G. When obtaining the density distributions, the matrix $[S]$ of the spectroscopic data shown in FIG. 4 were used. Since the matrix $[S]$ was measured by using samples

having the densities of 50 percents, the obtained component patterns were multiplied by 50 percents to estimate the densities.

FIG. 7A shows the density distribution of 5-aspirine,
5 FIG. 7B shows the density distribution of palatinose, FIG.
7C shows the density of riboflavin that was not contained
in the objects 10, and FIG. 7D shows the density
distribution of paper, plastic and so on that does not have
wavelength dependence of absorbancy. From these figures,
10 it is understood that the obtained density distributions
depend on the components of the respective pellets
constituting the objects 10. In other words, it is
understood that the density difference as well as the
components difference are extracted.

15 According to the method and apparatus of the present
invention, the tera-hertz wave generation device 12
generates the tera-hertz waves 4 of the different
wavelengths, the two-dimensional scan device 18 two-
dimensionally scans the objects 10 with the tera-hertz
20 waves, the spectroscopic measurement device 14 measures the
two-dimensional distribution [I] of the absorbance of the
objects, and the target density calculation device 16
calculates the two-dimensional distribution of the target
density P by imaging spectroscopy on the basis of the pre-
25 measured spectrum [S] of the target absorbance S and the
two-dimensional distribution [I] of the absorbancy I.

Accordingly, when the object is a mail article that includes a target having wavelength-dependent property of tera-hertz wave absorbancy, it is possible to determine the component of the object included in the mail article 5 without opening the mail article. Further, it is possible to detect abnormality of the object included in the mail article that was not detected by the conventional X ray photograph.

Furthermore, the device of the present invention 10 includes the image display device 20 that two-dimensionally displays the two-dimensional distribution of the target density P. Thereby, the shape of the target having wavelength-dependent property of tera-hertz wave absorbancy included in the mail article can be displayed two-dimensionally together with the target density distribution. 15

According to the present invention, difference in component such as a chemical agent is extracted as a spatial pattern from a set of images measured by tera-hertz waves of different wavelengths, using known tera-hertz wave 20 spectroscopic data. Thereby, it is possible to distinguish a component pattern of a material inside a parcel, an envelope, an opaque plastics container or the like.

Thus, the target inspecting method and apparatus using tera-hertz spectroscopic measurement has an excellent 25 advantage in that an inside component and its shape that were not determined by the X ray photograph can be

determined without opening the mail article.

The present invention is not limited to the above-described embodiment, and various modifications can be made without departing from the scope of the present invention.